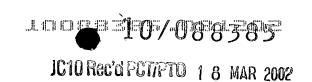


(Rev. 12-29-99)	_	ATTORNEY'S DOCKET NO. H 4193 PCT/US							
DESIGNATED/ELECTED OFFI	CE (DO/EO/US)	U.S. APPLICATION NO. (4) KNOWN See 37 CFR 1.5) 3 3 8 5							
INTERNATIONAL APPLICATION NO. PCT/EP00/08772									
TITLE OF INVENTION METHOD FOR PRODUCIN	G ALKYL-SUBSTITUTED BU	JTENOLS							
APPLICANT(S) FOR DO/EO/US  Lothar Friesenhagen, Step	bhan Heck, Norbert Klein, Ti	nomas Markert, Gerrit Pelzer							
Applicant herewith submits to the United St	ates Designated/Elected Office (EO/DO/US) t	he following items and other information:							
1. This is a FIRST submission of ite	erns concerning a filing under 35 U.S.C. 371.								
2.   This is a SECOND or SUBSEQUENCE.	JENT submission of items concerning a filing	under 35 U.S.C. 371.							
4. A proper Demand for International	al Preliminary Examination was made by the 19	oth month from the earliest claimed priority date.							
<ul><li>a.  is transmitted herewith (r</li><li>b.  has been transmitted by</li></ul>	equired only if not transmitted by the Internatio the International Bureau.								
6. A translation of the International Ap	plication into English (35 U.S.C. 371(c)(2)).								
<ul> <li>a.</li></ul>	(required only if not transmitted by the Internat the International Bureau. vever, the time limit for making such amendme	ional Bureau). ` ` ' '							
8.   A translation of the amendments to	the claims under PCT Article 19 (35 U.S.C. 3	71(c)(3)).							
9. An oath or declaration of the inventor	or(s) (35 U.S.C. 371(c)(4)). (UNEXECUTED)								
10. ☐ A translation of the annexes to the I	nternational Preliminary Examination Report u	nder PCT Article 36 (35 U.S.C. 371(c)(5)).							
12. ☐ An assignment document for record	ding. A separate cover sheet in compliance wi	th 37 CFR 3.28 and 3.31 is included.							
13. ■ A FIRST preliminary amendment  □ A SECOND or SUBSEQUENT pre	liminary amendment.								
14.   A substitute specification.									
15.   A change of power of attorney and/	or address letter.								
16. ☐ Other items or information:									
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Independent Claims	1-3=	0	0 X \$84.00	\$	0	
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PATENT Docket No. H 4193 PCT/US

## IN THE UNITED STATES PATENT AND TRADEMARK OFFICE

RE:

PCT/EP00/08772

International Filing Date: September 8, 2000 Priority Date Claimed: September 17, 1999

Applicant: Friesenhagen, et al.

Title: METHOD FOR PRODUCING ALKYL-SUBSTITUTED BUTENOLS

Applicants' Reference: H 4193 PCT/US

## **PRELIMINARY AMENDMENT**

Commissioner for Patents Box PCT Washington, DC 20231

Sir:

Before examination, in the national stage for the United States, of the above-captioned application under the Patent Convention Treaty, please amend as follows the translation supplied herewith of the application:

## In the Specification:

Please delete all text above line 8, of page 1, and replace the deleted matter with the following new section headings and new paragraph:

## --TITLE OF THE INVENTION

Method for Producing Alkyl-Substituted Butenols
BACKGROUND OF THE INVENTION

This invention relates to a process for the production of alkyl-substituted butenols by reduction of the corresponding aldehyde precursor in the presence of copper/zinc catalysts, the process being carried out continuously under isothermal conditions in a narrow temperature range.—

On a separate, new page 16, following page 15, please add the following new section heading and paragraph containing an Abstract of the Disclosure:



# Preliminary Amendment of U.S. National Stage for International Application PCT/EP00/08772 filed on September 8, 2000

## -- ABSTRACT OF THE DISCLOSURE

Alkyl-substituted butenols having the formula (I):

$$R^1$$
-CH<sub>2</sub>-CH=CR<sup>2</sup>-CH<sub>2</sub>OH (I)

wherein R¹ is a saturated or olefinically unsaturated alkyl or cycloalkyl group having from 4 to 16 carbon atoms and wherein R¹ is optionally substituted by an alkyl, cycloalkyl, aryl or alkaryl having up to 12 carbon atoms; R² is hydrogen or an alkyl group having from 1 to about 6 carbon atoms are produced by a process which comprises: (1) reacting an aldehyde of the formula (II):

$$R^1$$
-CH<sub>2</sub>-CHO (II)

wherein R¹ has the same meaning as in formula (I), with the corresponding lower aldehyde to form an unsaturated aldehyde in an inert organic solvent; (2) continuously contacting an optionally calcined copper/zinc catalyst with the unsaturated aldehyde under isothermal conditions at temperatures of from about 45 to about 60°C and under a hydrogen pressure of from 1 to about 300 bar.--

### In the claims:

Please cancel claims 1-9.

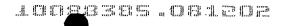
Please add the following new claims 10-17.

10. (New) A process for the production of alkyl-substituted butenols having the formula (I):

$$R^1$$
-CH<sub>2</sub>-CH=CR<sup>2</sup>-CH<sub>2</sub>OH (I)

wherein R<sup>1</sup> is a saturated or olefinically unsaturated alkyl or cycloalkyl group having from 4 to 16 carbon atoms and wherein R<sup>1</sup> is optionally substituted by an alkyl, cycloalkyl, aryl or alkaryl having up to 12 carbon atoms; R<sup>2</sup> is hydrogen or an alkyl group having from 1 to about 6 carbon atoms the process comprising the steps of: (1) reacting an aldehyde of the formula (II):

wherein R<sup>1</sup> has the same meaning as in formula (I), with the corresponding lower aldehyde to form an unsaturated aldehyde in an inert organic solvent; (2) continuously contacting an optionally calcined copper/zinc catalyst



# Preliminary Amendment of U.S. National Stage for International Application PCT/EP00/08772 filed on September 8, 2000

with the unsaturated aldehyde under isothermal conditions at temperatures of from about 45 to about 60°C and under a hydrogen pressure of from 1 to about 300 bar.

- 11. (New) The process of claim 10 wherein step (1) is carried out in a nonpolar organic solvent which can form an azeotrope with water.
- 12. (New) The process of claim 10 wherein step (1) is carried out in the presence of a catalyst which is an ammonium salt of an organic acid.
- 13. (New) The process of claim 10 wherein R<sup>2</sup> in formula (I) is a methyl group.
- 14. (New) The process of claim 10 wherein the lower aldehyde is propionaldehyde.
- 15. (New) The process of claim 14 wherein the propional dehyde is used in a 2.5 to 10-fold molar excess based on the aldehyde of formula (II).
- 16. (New) The process of claim 10 wherein R<sup>1</sup> is a 4-(2,2,3-trimethylcyclopent-3-en-1-yl) group.
- 17. (New) The process of claim 10 wherein the organic solvent selected from the group consisting of toluene, xylene, benzene, cyclohexane and methyl cyclohexane.



# Preliminary Amendment of U.S. National Stage for International Application PCT/EP00/08772 filed on September 8, 2000

## **REMARKS**

Claims 10-17 are currently pending in the instant application.

The Specification has been amended to include the preferred section headings pursuant to 37 C.F.R. §1. It is submitted that the amendments to the Specification made herein introduce no new matter. Their entry is therefore proper and respectfully requested. An Abstract of the Disclosure has been added on a separate sheet following the claims.

Original claims 1-9 have been canceled and replaced with new claims 10-17 solely for the purpose of improving clarity and grammar, which may suffer in translation, and not for any reason related to the statutory requirements for a patent. New claims 10-17 have not been added in response to any rejection, or in anticipation of any rejection related to the statutory requirements for a patent. Applicants respectfully submit that the scope of new claims 10-17 corresponds to the scope of original claims 1-9 and that new claims 10-17 are no narrower than original claims 1-9. Furthermore, although a moot point in view of their cancellation, Applicants respectfully submit that original claims 1-9 satisfied the requirements of 35 U.S.C. §112, as filed. New claims 10-17 are supported by the specification and no new matter has been introduced. Entry is therefore proper and respectfully requested. Prompt examination of the instant application in view of the amendments made herein is respectfully requested.

Respectfully submitted,

J6hn E. Drach

(Reg. No. 32,891)

Attorney for Applicants

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PCT/EP00/08772

# Method for Producing Alkyl-Substituted Butenols

## Field of the Invention

This invention relates to a process for the production of alkylsubstituted butenols by reduction of the corresponding aldehyde precursor in the presence of copper/zinc catalysts, the process being carried out continuously under isothermal conditions in a narrow temperature range.

#### **Prior Art**

Judging by demand, the availability of many natural perfumes is totally inadequate. From the perfumistic point of view, sandalwood oil is rated particularly highly and is of great value. It is obtained by steam distillation from the heartwood of the sandalwood tree, a tropical semiparasite which occurs in India and Malaysia. Heartwood appears after about 10 years and only begins to develop relatively quickly in 20-year-old trees. Fully grown trees are uprooted at the age of 30 to 60 because the roots are particularly rich in fragrant heartwood [cf. E.T. Morris, Dragoco Report 1983 (30), 40]. It will therefore be appreciated why perfume researchers are constantly endeavoring to develop suitable substitutes for natural sandalwood oil.

The focal points in the development of suitable substitutes for natural sandalwood oil were outlined by R.E. Naipawer in a review [in: B.M. Lawrence, B.D. Mookherjee, B.J. Willis (Eds.): "Flavors and Fragrances: A World Perspective", Elsevier Publishers, Amsterdam 1988]. In this review, it is mentioned inter alia that, since the middle of the seventies, campholenyl derivatives have played an important part as synthetic perfumes with a sandalwood perfume. A key role in this access to synthetic sandalwood perfumes has been played by the fact that campholene aldehyde (B), the synthesis building block on which the

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compounds mentioned are based, can readily be obtained from  $\alpha$ -pinene, a natural substance.

2-Alkyl-4-(2,2,3-trimethylcyclopent-3-enyl)-but-2-en-1-ols (A), hereinafter referred to as **sandalols**, are sought-after perfumes with a pronounced sandalwood fragrance.

Cy = 4-(2,2,3-trimethylcyclopent-3-en-1-yl) group R = H or  $C_{1-6}$  alkyl

JP-A2-55/036423 (reported in Chem. Abstr. 93/094886p) describes a process for the production of such a sandalol in which α-campholene aldehyde (B) is reacted with propionaldehyde (CH<sub>3</sub>-CH<sub>2</sub>-CHO) in the presence of sodium hydroxide as basic catalyst.

The unsaturated aldehyde (C) formed in this mixed aldol condensation was isolated in a yield of 73.5%.

Cy-CH<sub>2</sub>-CH=C(CH<sub>3</sub>)-CHO (A)
$$Cy = 4-(2,2,3-trimethylcyclopent-3-en-1-yl) group$$

Finally, in another step, this unsaturated aldehyde (C) was reduced with Al[OCH(CH<sub>3</sub>)]<sub>3</sub> to form the corresponding sandalol (A). The yield obtained is put at 85%.

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**DE-A-195 20 103** describes a process for the production of alkyl-substituted butenols where unsaturated aldehydes are prepared by aldol condensation in a first step and are subsequently reduced in the presence of an optionally calcined copper/zinc catalyst. Example 3 of this application (page 5, lines 5 to 26), which describes the second stage of the process (reduction step), refers to batch operation and a reaction temperature of 160°C.

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Continuous operation in an extremely narrow and relatively low temperature range is neither disclosed nor suggested in DE-A-195 20 103. Isothermal operation is also not mentioned in DE-A-195 20 103.

## **Description of the Invention**

The known processes for the production of sandalols (A) are not entirely satisfactory in regard to yield and economy. Accordingly, there was a need for an improved process for the production of the compounds (A) and analogous compounds where the "Cy" group would be replaced by another saturated or olefinically unsaturated, optionally substituted alkyl or cycloalkyl group. More particularly, there was a need to ensure that the nonspecific formation of numerous secondary products would largely be avoided. Secondary products in a perfumistic context are understood to be worthless or even troublesome products.

It has now been found that alkyl-substituted butenols corresponding to general formula (I):

$$R^{1}-CH_{2}-CH=CR^{2}-CH_{2}OH \qquad (I)$$

in which R<sup>1</sup> is a saturated or olefinically unsaturated alkyl or cycloalkyl group containing 4 to 16 carbon atoms which may optionally be substituted by an alkyl, cycloalkyl, aryl or alkaryl group, with the proviso that this substituent contains at most 12 carbon atoms, and R<sup>2</sup> is hydrogen or an

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alkyl group containing 1 to 6 carbon atoms, can be produced in high yields providing the aldol condensation of aldehydes corresponding to formula (II):

5  $R^1$ -CH<sub>2</sub>-CHO (II)

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in which R<sup>1</sup> has the same meaning as in formula (I), and the corresponding lower aldehyde is carried out in an inert organic solvent and the unsaturated aldehydes obtained are reduced in the presence of an optionally calcined copper/zinc catalyst, the process being carried out continuously under isothermal conditions in a narrow temperature range.

Accordingly, the present invention relates to a process for the production of alkyl-substituted butenols corresponding to general formula (I):

 $R^1$ -CH<sub>2</sub>-CH=CR<sup>2</sup>-CH<sub>2</sub>OH (I)

in which R<sup>1</sup> is a saturated or olefinically unsaturated alkyl or cycloalkyl group containing 4 to 16 carbon atoms which may optionally be substituted by an alkyl, cycloalkyl, aryl or alkaryl group, with the proviso that this substituent contains at most 12 carbon atoms, and R<sup>2</sup> is hydrogen or an alkyl group containing 1 to 6 carbon atoms,

by reacting aldehydes corresponding to formula (II):

 $R^{1}-CH_{2}-CHO (II)$ 

in which R<sup>1</sup> has the same meaning as in formula (I), with the corresponding lower aldehydes and subsequently reducing the unsaturated aldehydes obtained.

30 i) the aldol condensation being carried out in an inert organic solvent

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and

(ii) the reduction of the unsaturated aldehydes being carried out in the presence of an optionally calcined copper/zinc catalyst,

with the proviso that the reduction in step ii) is carried out continuously under isothermal conditions at temperatures of 45 to 60°C and under a hydrogen pressure of 1 to 300 bar.

The process according to the invention has the advantage over the prior art that intermediate products and valuable products are obtained in high purities and in substantially quantitative yields. In particular, it has the advantage that the valuable product (I) obtained in the hydrogenation step is formed with a very high chemical purity and selectivity. Of particular importance in this connection is the fact that unwanted secondary products, for example compounds derived from (I) of which the C=C double bonds are completely or partly hydrogenated, and unreacted aldehyde (from the aldol condensation), are formed in a distinctly reduced quantity by comparison with processes where the features to be observed in accordance with the invention do not exist. This is particularly of advantage when the valuable product (I) obtained in the hydrogenation step is used as a raw material for the production of perfumes.

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## Step i)

Particularly suitable inert organic solvents for step i) are nonpolar solvents which form an azeotrope with water. Examples of suitable solvents are toluene, xylene, benzene, cyclohexane and methyl cyclohexane.

In a special embodiment of the invention, ammonium salts of an organic acid are used to catalyze the aldol condensation.

Propionaldehyde is preferably used in a 2.5- to 10-fold molar excess, based on the aldehyde (II). In one particular embodiment, propionaldehyde is used in a 2.5- to 3.5-fold molar excess.

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As already mentioned, the aldol condensation is preferably carried out in the presence of an ammonium salt of an organic acid in the process according to the invention. Basically, the nature of the acid is not critical. Nor does it matter whether the ammonium salt is used as such or whether it is formed in situ during the reaction - for example from an amine and an organic acid. Examples of suitable ammonium salts are benzyl trimethyl ammonium hydroxide, piperidinyl acetate, pyrrolidinium acetate. ammonium acetate, dimethyl ammonium pyridinyl acetate, morpholine acetate, Lewatit 11600 (active with acetic acid), piperidinyl formate, N,Ntetraacetyl ethylenediamine, N,N-diacetyl ethylenediamine, dibutyl ammonium acetate and piperidinyl propionate. The concentration of the catalyst is preferably in the range from 0.001 to 20 mole-% and more particularly in the range from 0.5 to 10 mole-%, based on the aldehyde (II) used.

In another preferred embodiment of the present invention, R<sup>1</sup> in general formula (I) is a 4-(2,2,3-trimethylcyclopent-3-enyl) group.

## Step ii)

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The process according to the invention is carried out at temperatures of 45 to 60°C. In one particularly preferred embodiment, the reaction temperature is in the range from 50 to 55°C.

The process according to the invention is distinguished inter alia by the fact that, in step ii), it is carried out both continuously and isothermally.

Carrying out the process according to the invention continuously in step ii), which is preferably carried out in a fixed-bed reactor, ensures that the proportion of secondary products is small. The reason for this on the one hand is that, where this procedure is adopted, it is readily possible by controlling the volumetric flow rate of aldehyde or aldehyde and solvent to keep the reaction time short. On the other hand, the heterogeneous catalysis applied here ensures that the reaction product is not accompanied by significant quantities of the catalyst.

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Carrying out the process isothermally means that no significant temperature gradients occur in the continuously operated reactor and that, in particular, there are no temperature peaks. By contrast, a nonisothermal reaction procedure would be characterized by the occurrence of distinct temperature gradients or temperature peaks in the reactor. Nonisothermal conditions usually prevail in batch hydrogenation, i.e. hydrogenation in an autoclave. In continuous operation, a nonisothermal reaction procedure would be characterized by the absence of special precautions to control the exothermy of the reaction.

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To establish isothermal conditions, a particular embodiment of the process according to the invention is characterized in that the temperature is controlled by external jacket heating, for example with thermal oil, and/or the throughflow rate is adjusted to a correspondingly high level.

In particular, the throughflow rate in step ii) is adjusted to a value of 0.5 to 1.5 m<sup>3</sup>/h and more particularly to a value of 0.8 to 1.2 m<sup>3</sup>/h.

A preferred embodiment of the invention is characterized in that the copper/zinc catalyst is used in particulate form, i.e. the catalyst which is used in the reaction zone of the fixed-bed reactor is in the form of solid particles (heterogeneous catalyst). The particles may assume various sizes and shapes, for example tablets, lumps, cylinders, rods, rings. Basically, the size of the particles is not critical. However, it is normally adapted to the particular reactor dimensions present so that the liquid phase and the carrier gas are able to pass through the reaction zone unhindered and no unwanted drop in pressure occurs in that region. Typical suitable particle sizes range from a mean diameter of ca. 1 millimeter to ca. 10 millimeters although larger or smaller particle sizes are also possible.

A typical laboratory apparatus for carrying out the process according to the invention comprises a fixed-bed reactor of a double-jacketed tube. The inner tube contains the heterogeneous hydrogenation catalyst and

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acts as the reaction zone. The intermediate space is used for heating with a liquid medium. The aldehyde or the mixture of aldehyde and solvent can be delivered continuously to the reactor through heatable pipes by a controllable piston diaphragm pump. After leaving the reactor, the reaction products formed can readily be quantitatively removed via a cooling unit and an expansion system.

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The typical technical equipment for carrying out the process according to the invention described with reference - by way of example - to a laboratory apparatus can readily be applied to correspondingly scaled up pilot-plant or production reactors. In principle, any of the usual tube or tube-bundle reactors may be used for this purpose.

So far as the hydrogen pressure is concerned, step ii) of the process is preferably carried out in the 200 to 300 bar range. Hydrogen pressures of 220 to 260 bar are particularly preferred.

The hydrogenation in step ii) is preferably carried out in the presence of a solvent. Alcoholic compounds, especially low molecular weight primary alkanols, such as methanol and/or ethanol, are particularly suitable solvents. The quantity ratio of aldehyde to solvent in step ii) of the process according to the invention is basically not critical although ratios by volume of aldehyde to solvent of 10:1 to 1:10 are preferred, a range of 3:1 to 1:1 being particularly preferred.

The copper/zinc catalysts to be used for the purposes of the invention are known from the prior art. They are prepared in accordance with **DE-A-42 42 466** by adding alkali metal carbonate compounds to aqueous solutions containing water-soluble copper(II) and zinc(II) salts up to a pH value of 6 to 10, removing and drying the deposit formed, calcining the dried catalyst for 1 to 60 minutes at temperatures of 400 to 600°C and then converting the calcined catalyst into particulate form. Further information on the production of the copper/zinc catalysts can be found in DE-A-42 42 466, page 3, lines 13 to 34.

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In order substantially to avoid further hydrogenation of the target product (I) to secondary products, it has proved to be favorable in the continuous reaction in a fixed-bed reactor to adjust the volumetric flow rate of the aldehyde to LHSV values which are preferably in the range from 0.3 to 3.0 h<sup>-1</sup> and more particularly in the range from 0.6 to 1.2 h<sup>-1</sup>. The LHSV value (liquid hourly space velocity) is understood from the literature to be the volumetric flow rate of the liquid, based on the volume of the solid catalyst. The LHSV values mentioned herein are based solely on the aldehyde, i.e. the solvent optionally used is disregarded.

The circulating gas volume is adjusted to values of 1 to 2 Dm<sup>3</sup>/h ("pressure cubic meters per hour"). By circulating gas volume is meant: m<sup>3</sup> circulating gas per hour for a reactor pressure of 250 to 300 bar. This parameter is measured in the pressure range of the reactor used (cf. Example 3 of the present application and the associated Fig. 1) after the gas circulation pump by means of a turbine.

For the purposes of the invention, the volumetric flow rate is normally adjusted to GHSV values in the range from 200 to 1,000 h<sup>-1</sup> and preferably to GHSV values in the range from 250 to 500 h<sup>-1</sup>. The GHSV value (gaseous hourly space velocity) is understood from the literature to be the volumetric flow rate of the carrier gas, based on the volume of the solid catalyst.

#### Examples

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### 1. Substances used

## 1.1. For the aldol condensation

α-campholene aldehyde: 85% (Glidco) propionaldehyde: 98% (Riedel-de-Häen)

30 KF on Al<sub>2</sub>O<sub>3</sub>: 240 g basic aluminium oxide were suspended in 320 g of a

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50% aqueous potassium fluoride solution and then concentrated to dryness in a water jet vacuum in a rotary evaporator. The catalyst was then dried for 4 hours at 130°C/50 mbar.

## 1.2. For the reduction of the unsaturated aldehyde

Copper/zinc catalyst: The copper/zinc catalyst used was prepared in accordance with Example A) of DE-A-42 42 466 using copper(II) nitrate trihydrate, zinc(II) nitrate hexahydrate and sodium carbonate.

10 2. The reactions

## 2.1. Aldol condensation

## Example 1

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## Quantities used:

3.04 g (20 moles)  $\alpha$ -campholene aldehyde

4.64 kg (80 moles) propionaldehyde400 g basic aluminium oxide charged with 40% potassium fluoride.

## Reaction procedure:

1.5 kg of a mixture (molar ratio 1:4) of campholene aldehyde and propionaldehyde was introduced into a 10-liter glass reactor. 400 kg of KF on Al<sub>2</sub>O<sub>3</sub> were added in portions under nitrogen (5 l/h) with vigorous stirring and cooling, the temperature of the reaction mixture being kept between 40 and 50°C. The remaining 6.2 kg of the aldehyde mixture were then continuously added under nitrogen with vigorous stirring at a rate of 2 liters per hour. The reaction was exothermic and was kept by cooling at 40°C. After the addition, the mixture was stirred overnight at 50°C, the campholene aldehyde reacting off completely.

## Working up:

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To remove the catalyst, the reaction mixture was pumped into a 2-

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liter pressure nutsche and filtered under 5 bar nitrogen. The filter cake was briefly washed with 0.5 liter of isopropanol. The crude product was returned to the reactor and ca. 270 g organic phase and 22 g water phase were distilled off at atmospheric pressure and at bottom temperatures of up to 150°C. The residue of 5.1 kg left in the reaction vessel was washed twice with 2 liters of saturated sodium sulfate solution. The residue of 5 kg remaining was further processed as a crude product (the content of 2-methyl-(2,2,3-trimethylcyclopent-3-en-1-yl)-but-2-en-1-al was found by gas chromatography to be 43%).

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## Example 2

## Quantities used:

3.04 kg (20 moles)  $\alpha$ -campholene aldehyde

2.9 kg (50 moles) propionaldehyde

15 170 + 85 g (3 moles) piperidine

120 + 60 g (3 moles) glacial acetic acid

2 kg toluene

#### Reaction procedure:

3.04 kg of campholene aldehyde and 2 kg of toluene were introduced into a 10-liter glass reactor and 2.9 kg of propionaldehyde, 170 g of piperidine and 120 g of glacial acetic acid were added with stirring at room temperature. The mixture was then refluxed for 4 hours on a water separator, 680 ml of water of reaction being removed from the circuit.

25 Analysis of a sample of the reaction mixture by gas chromatography revealed a percentage content of 15% of unreacted educt. Accordingly, another 85 g of piperidine and 60 g of glacial acetic acid were added. After refluxing for another hour, another 120 g of water were removed from the circuit and the educt was completely reacted.

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## Working up:

After 1.9 kg of toluene had been distilled off, the reaction mixture was washed twice with 2 liters of water. The organic phase of 6.24 kg was distilled in a 30 cm packed column (boiling point 88-102°C/0.1 mbar), 3.27 kg of a yellowish colored product (gas-chromatographic purity 85%) being obtained (85% of the theoretical).

## 2.2. Reduction

## Example 3 (invention)

## 10 Apparatus:

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A jacketed high-pressure reactor filled with a Cu/Zn catalyst was used. It was connected to the following units: high-pressure product pump, heater, cooler, separator and gas circulation pump. The heat carrier circuit was controlled by a temperature-controllable apparatus. The layout of the apparatus used in schematized in Fig. 1.

## List of reference numerals in Fig. 1

- educt (crude product of the aldol condensation of Example 2) / methanol
- 20 2 high-pressure product pump
  - 3 heater
  - 4 reactor (jacketed)
  - 5 heat carrier oil
  - 6 cooler
- 25 7 separator
  - 8 gas circulation pump
  - 9 hydrogen supply ("fresh H<sub>2</sub>")

### Quantities used:

30 24.7 kg crude product of the aldol condensation of Example 2 (= educt)

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10.5 kg methanol, technical quality (= solvent) 26 kg Cu/Zn catalyst

## Reaction procedure:

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After it had been filled with the catalyst, the reactor was closed and tested for leaks with 250 bar hydrogen pressure. The catalyst was then activated by continuous introduction of hydrogen under a reactor pressure of 50 bar N2 and at a temperature increased by 5°C per hour, a final temperature of 200°C being established. The circulating gas volume was kept at 1.5 Dm<sup>3</sup>/h. The end of activation of the catalyst, as reflected in an H<sub>2</sub> content in the circulating gas of more than 5%, i.e. the catalyst did not take up any more hydrogen, was followed by gas exchange in the reactor. To carry out the hydrogenation process, 250 bar hydrogen was introduced into the reactor after the complete expansion of hydrogen and the catalyst bed was adjusted to 50-55°C through the hydrogen, reactor entry and heat carrier temperature. The circulating gas volume was 2 Dm<sup>3</sup>/h. After the operating parameters had stabilized, the addition of a mixture of 2 parts by volume of the crude product of the aldol condensation of Example 2 (= educt) and 1 part by volume of methanol (= solvent) was started at 10 l/h, rising gradually to 40 l/h. After all the mixture had been added, the educt/hydrogen mixture showed a reactor entry temperature and heat carrier oil exit temperature of 55°C. The exothermy in the reactor was 5 to 10°C. After cooling, the hydrogenation product and the hydrogen were separated in a separator, the hydrogen was fed to the gas circulation pump and the end product was removed through an automatic expansion system. The crude product obtained in this way was then characterized by gas chromatography. It contained 86% of the required valuable product, 12% of a perfumistically attractive accompanying product and 1.8% of unreacted educt. Hardly any of the secondary products formed, for example, at higher temperatures or in batch operation were detected.

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#### **CLAIMS**

1. A process for the production of alkyl-substituted butenols corresponding to general formula (I):

5 R<sup>1</sup>-CH<sub>2</sub>-CH=CR<sup>2</sup>-CH<sub>2</sub>OH

**(I)** 

in which R¹ is a saturated or olefinically unsaturated alkyl or cycloalkyl group containing 4 to 16 carbon atoms which may optionally be substituted by an alkyl, cycloalkyl, aryl or alkaryl group, with the proviso that this substituent contains at most 12 carbon atoms, and R² is hydrogen or an alkyl group containing 1 to 6 carbon atoms,

by reacting aldehydes corresponding to formula (II):

R¹-CH<sub>2</sub>-CHO (II)

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in which R<sup>1</sup> has the same meaning as in formula (I), with the corresponding lower aldehydes and subsequently reducing the unsaturated aldehydes obtained,

- i) the aldol condensation being carried out in an inert organic solvent and
- (ii) the reduction of the unsaturated aldehydes being carried out in the presence of an optionally calcined copper/zinc catalyst,

characterized in that the reduction in step ii) is carried out continuously under isothermal conditions at temperatures of 45 to 60°C and under a hydrogen pressure of 1 to 300 bar.

- 2. A process as claimed in claim 1, characterized in that the aldol condensation is carried out in a nonpolar organic solvent which forms an azeotrope with water.
- 3. A process as claimed in claim 1 or 2, characterized in that the aldol condensation is carried out in the presence of an ammonium salt of an

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organic acid as catalyst.

- 4. A process as claimed in any of claims 1 to 3, characterized in that R<sup>2</sup> in formula (I) is a methyl group.
- 5. A process as claimed in claim 4, characterized in that propionaldehyde is used in a 2.5 to 10-fold molar excess, based on the aldehyde (II), in step i).
  - 6. A process as claimed in any of claims 1 to 5, characterized in that R<sup>1</sup> is a 4-(2,2,3-trimethylcyclopent-3-en-1-yl) group.
- 7. A process as claimed in any of claims 1 to 6, characterized in that an organic solvent selected from the group consisting of toluene, xylene, benzene, cyclohexane and methyl cyclohexane in used in step i).
  - 8. The use of the alkyl-substituted butenols of formula (I), in which R<sup>1</sup> is a saturated or olefinically unsaturated alkyl or cycloalkyl group containing 4 to 16 carbon atoms which may optionally be substituted by an alkyl, cycloalkyl, aryl or alkaryl group, with the proviso that this substituent contains at most 12 carbon atoms, and R<sup>2</sup> is hydrogen or an alkyl group containing 1 to 6 carbon atoms, produced by the process claimed in any of claims 1 to 7 as perfumes.
- 9. The use claimed in claim 8 in cosmetic preparations, technical20 products or alcohol-based perfumery.



## ABSTRACT OF THE DISCLOSURE

Alkyl-substituted butenols having the formula (I):

$$R^{1}-CH_{2}-CH=CR^{2}-CH_{2}OH \qquad (I)$$

wherein R¹ is a saturated or olefinically unsaturated alkyl or cycloalkyl group having from 4 to 16 carbon atoms and wherein R¹ is optionally substituted by an alkyl, cycloalkyl, aryl or alkaryl having up to 12 carbon atoms; R² is hydrogen or an alkyl group having from 1 to about 6 carbon atoms are produced by a process which comprises: (1) reacting an aldehyde of the formula (II):

wherein R¹ has the same meaning as in formula (I), with the corresponding lower aldehyde to form an unsaturated aldehyde in an inert organic solvent; (2) continuously contacting an optionally calcined copper/zinc catalyst with the unsaturated aldehyde under isothermal conditions at temperatures of from about 45 to about 60°C and under a hydrogen pressure of from 1 to about 300 bar.



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PATENT AP	PLICATION	Application Number	10/088,3	10/088,385				
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Type a plus sign (+) inside this box H 4193 PCT/US ADDITIONAL INVENTOR(S) **DECLARATION** Supplemental Sheet Name of Additional Joint Inventor, if any: A petition has been filed for this unsigned inventor Suffix Middle Family **Schneider** Markus Name e.g. Jr. Initial Name Date 04/25/02 Inventor's Signature Citizenship Residence: Duisburg State Country Germany City Post Office Address Zum Holzenberg 9 Post Office Address Applicant State Zip Country Germany 47279 Duisburg City Authority Name of Additional Joint Inventor, if any: A petition has been filed for this unsigned inventor Suffix Middle Family Given e.g. Jr. Initial Name Name Date Inventor's Signature Citizenship Residence: State Country City Post Office Address Post Office Address Country Applicant State Zip City Authority Name of Additional Joint Inventor, if any: A petition has been filed for this unsigned inventor Suffix **Family** Middle Given Name e.g. Jr. Initial Name Date **Inventor's** Signature State Country Citizenship Residence: Post Office Address Post Office Address Applicant Zip Country State Authority Name of Additional Joint Inventor, if any: A petition has been filed for this unsigned inventor Suffix Middle Given e.g. Jr. Initial Name Name Date Inventor's Signature Citizenship State Country Residence: City Post Office Address Post Office Address Applicant Country State Zip City Authority Additional inventors are being named on supplemental sheet(s) attached hereto